

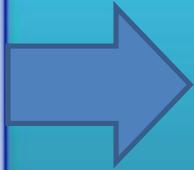
WELCOME TO MY PRESENTATION

***SUB: TRANSMISSION AND DISTRIBUTION OF ELECTRICAL
POWER-1***

SUB CODE:26762(6TH ELECTRICAL)

***Md . Abdul Matin Sarker
Instructor (electrical)
Rangpur Polytechnic institute***

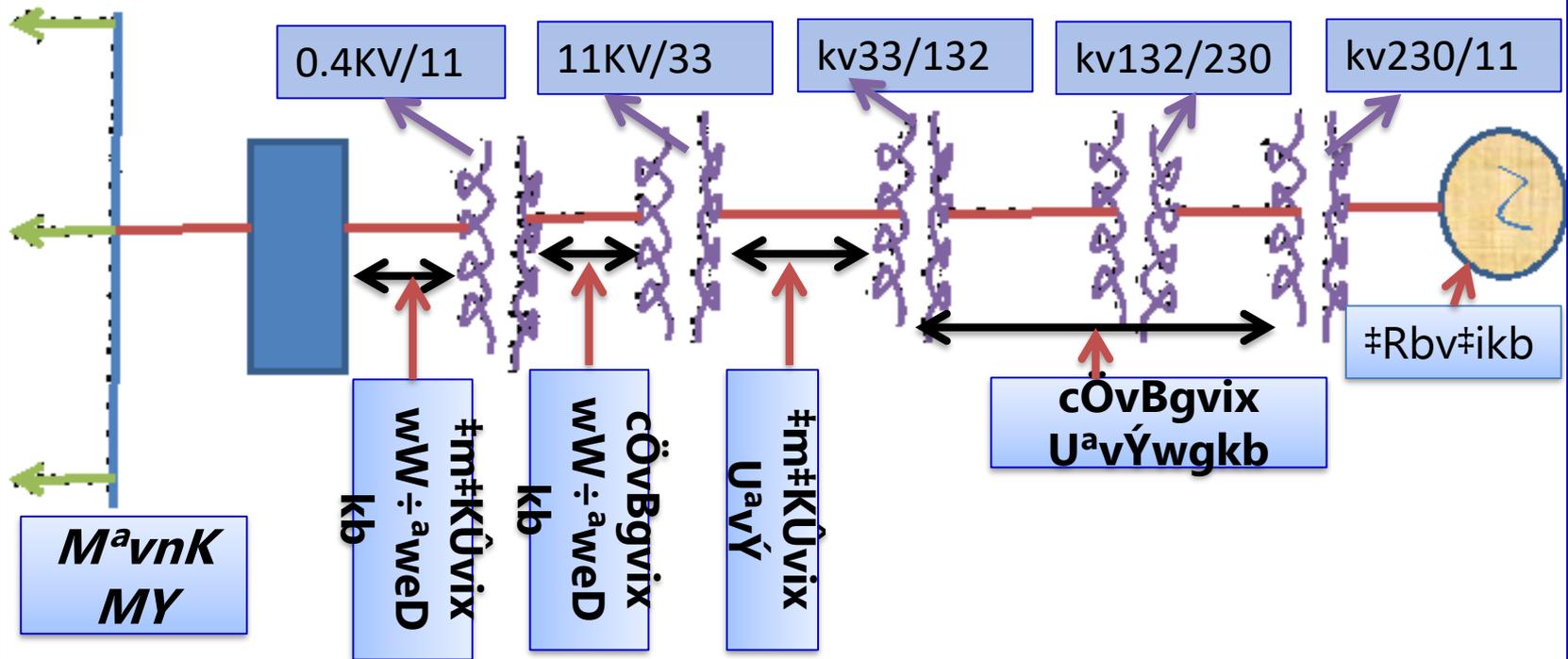
Aaävq -01



B‡jKwU^aKvj Gbvwr© U^avÝwgkb I
wWw÷^aweDk‡bi eävLüt-



Drcv`b †K>`a ‡_‡K AvevwmK feb ch©šÍ we`yř
†cŠQv‡bvi wbwg‡Ë cwievwn Zv‡ii GK wekvj
†bUIqvK© eävZ nq| ZvB Drcv`b †K>`a †_‡K MÖvnK
ch©v‡q we`yř †cŠQv‡bvi wewfbœ avc,‡jv
Gbvwr© U^avÝwgkb GÛ wWw÷^aweDk‡bi AšÍf©y³|
wb‡œ Gbvwr© U^avÝwgkb I wWw÷^aweDkb
wewfbœ avc,‡jv †`Lv‡bv njt



eøK WvqvMÖvg Ad `v UªvÝwgkb GÛ

wWw:ªweDkb wm#:g

U^avÝwgkb jvBbt Drcv`b #K+>`^ai †cÖiY cÖvší

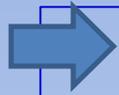
†_#K wewfboe mve-#÷kb ch©ší D" P cvIqvi
cwien#bi Rb`th wekvj †bUIqvK© eëüZ nq ,

Zv#K U^avÝwgkb jvBb e#j| Bnv `yB cÖKvi,

1| cÖvBgvix U^avÝwgkbt **230#Kwf, 132 †Kwf**

2| †m#KÛvix U^avÝwgkb t **66 †Kwf , 33**

†Kwf|



wWw ÷^aweDkb jvBb t mve-÷kb †_#K

MÖvnK ch©šÍ A_v©r AvevwmK feb, wkí-

KviLvbv wK^α^v evwbwRĶ GjvKvq we`yř

weZi#bi Rb`th †bUIqvK© eëüZ nq , Zv#K

wWw ÷^aweDkb jvBb e#j|

wWw ÷^aweDkb wm#÷g Avevi `yB ai#bi

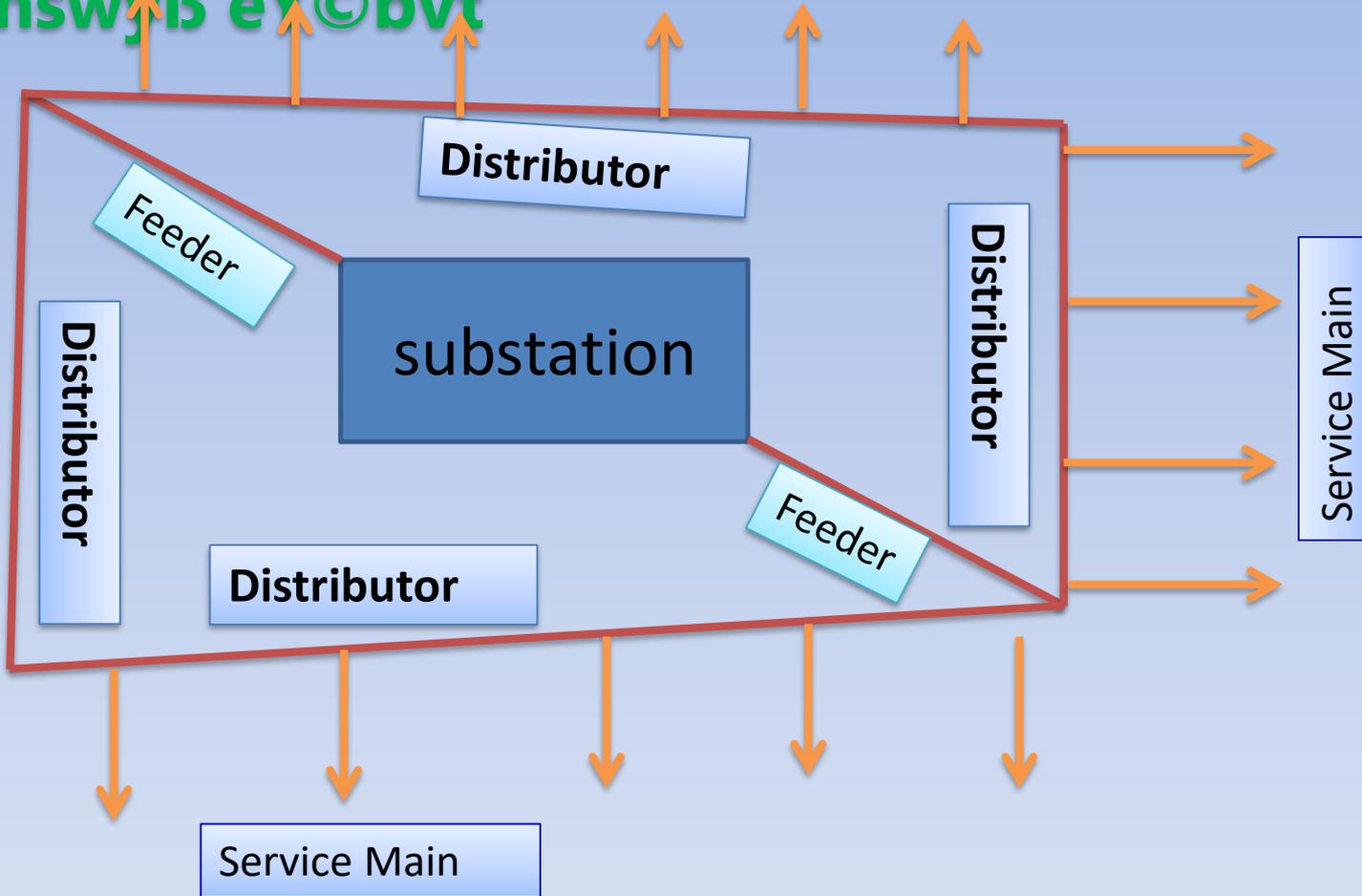
1| cÖvBgvix wWw ÷^aweDkb 11 †Kwf, 6.6

†Kwf, 3.3#Kwf

2| †m#KÛvix wWw ÷^aweDkb 400 †fvë, 230

†fvë |

1.2 $w d W v i$, $w W w \div ^a w e D U i$, $m v w f \textcircled{m} \dagger g B b G i$ $m s w j \beta e Y \textcircled{b} v t$





wdWvi t Rbeûj GjvKvi mwnZ †Rbv#iwUs †÷k#bi
ms#hvM mvabKvix †gvUv cwievnx Kÿej#K wdWvi
e#j A_ev mve#÷kb †_#K Rbeûj GjvKvi U^avÝdigv#ii
cÖvBgvix ch©šÍ ms#hvM mvabKvix †gvUv
cwievnx Kÿej#K wdWvi e#j|

wWw÷^aweDUit Rbeûj GjvKvi U^avÝdigv#ii
†m#KÛvix †_#K †h jvBb †ei n#q hvq Ges D³ jvBb
cwievnx †_#K Uÿwcs K#i MÖvn#Ki wgUv#i ms#hvM
†`Iqv nq, D³ cwievnx#K wWw÷^aweDUi e#j|



mvwf©m †gBbt †h Kve‡ji
gva‡g wWw÷^aweDUi †_‡K
Uüwcs K‡i M^avnK‡`i
mvcøvB †`Iqv nq, Zv‡K
mvwf©m †g&Bb e‡j|



1.4 Gwm I wWwm U^avÝwgk[#]bi g[#]a^{..} cv ©K^{..}wb^æœiæct

Gwm U^avÝwg[̄]kb

wWwm U^avÝwgk^b

1| wZb Zvi cÖ[#]qvRb Ges
Zvgvi LiP †ekx
2| BÛvK[#]UÝ, KücvwmUi,
cvIqvi d^v±i Ges mv[#]R©i
cÖfve we`g^vb |
3| w[̄]<b B[#]d± we`g^vb|
4| Bnvi cwienb K^ve[#]j
Bbmy[#]jkb †ekx jv[#]M|
5| †fv[#]ëR †i[,]jkb wb^æœgv[#]bi|
6| †fv[#]ëR[#]K †÷c Avc Ges
†÷c-WvDb Kiv hvq|

1| `yBZvi jv[#]M ZvB Zvgvi LiP
Kg|
2| Bnv[#]Z Gm[#]ei cÖfve †bB|
3| Bnv[#]Z w[̄]<b B[#]d± †bB|
4| Bnv[#]Z Bbmy[#]jkb Kg
jv[#]M|
5| †fv[#]ëR †i[,]jkb DbœZ|
6| D³ cwien[#]b †fv[#]ëR[#]K †÷c-
Avc Ges †÷c- WvDb Kiv hvq
bv|

1.5 Ifvi#nW Ges AvÛviMÖvDÛ wm#÷g Gi g#a`Zzjbv t

Ifvi#nW wm#÷g

- 1| Ifvi#nW jvBb mvavibZt
KvV/Ks&wµU/óxj †cvj A_ev
UvIqv#i Bbmy#jU#ii gva#g
Szjv#bv _v#K|
- 2| cÖv_wgK LiP Kg|
- 3| iyYv#eÿY LiP ZzjbvgyjK
†ekx|
- 4| KÛv±i ´úvwms †ekx _v#K
e#j jvB#b †fv#ëR W^ac †ekx
nq|
- 5| mvR© †fv#ëR
cÖwZ#ivwa eë´v wb#Z nq|

AvÛviMÖvDÛ wm#÷g

- 1| Bnv KÛzBU ev †U^a#Âi g#a`
w`#q wb#q hvIqv nq|
- 2| Bnv#Z cÖv_wg&K LiP
†ekx|
- 3| iyYv#eÿY LiP Kg|
- 4| KÛv±i ´úvwms Kg _v#K
e#j jvB#b †fv#ëR W^ac Kg nq|
- 5| Bnv#Z eë´v wb#Z nq|

$mgxKi\#bi\ mnv\#h\ \cdot\ \text{Lvl}\ \#h, D''P\ \#fv\#e\#R\ cvIqvi$
 $U^a\ v\acute{Y}wgk\#b\ cwievnx\ AvqZb\ Kg\ jv\#M\ Ges\ \grave{y}Zv\ \#tekx$
 $cvIqvi\ #jv\#$

$\#fv\#e\#RU^a\ v\acute{Y}wgk\#bi\ Zyjbvqnv\ B\ \#fv\#e\#RU^a\ v\acute{Y}wgk\#bi\ myweavt$

$1\ | D''P\ \#fv\#e\#R\ cvIqvi\ U^a\ v\acute{Y}wgk\#b\ cwievnx\ AvqZb$
 $Kg\ jv\#M\ |$

$2\ | D''P\ \#fv\#e\#RU^a\ v\acute{Y}wgk\#bjv\ B\ \#bi\ \grave{y}Zve\text{,,}w\times\ cvq\ |$

$c\ddot{O}gvYt\ 1\ | D''P\ \#fv\#e\#R\ cvIqvi\ U^a\ v\acute{Y}wgk\#b\ cwievnx\ AvqZb\ Kg$
 $jv\#Mt$

$awi, wZb\#dRGwm\ U^a\ v\acute{Y}wgk\#bcvIqvi = P\ \text{Watt}$

$jvB\ \#fv\#e\#R = V\ \text{volt}$

$\#jvW\ cvIqvi\ d\ddot{v}\ \pm\ i = \cos\ \emptyset$

$U^a\ v\acute{Y}wgk\#bjv\ B\ \#bi\ \text{N}\ \text{C}'' = L\ m$

$c\ddot{O}w\ Z\ Zv\ \#ii\ \#iva = R\ \Omega$

$cwievnx\ Zv\ \#ii\ Av\ \#cw\ \#K\ \#iva = \rho\ \Omega\text{-m}$

$cwievnx\ Zv\ \#ii\ c\ddot{O}\ \text{''}\ \#''\ Q\ ` = A\ sq\text{-m}$

$$W = \sqrt{3} V I \cos \phi, \quad R = \frac{\rho l}{A}$$

$$W = 3 I^2 R = 3 \left(\frac{p}{\sqrt{3} V \cos \phi} \right)^2 \times \frac{\rho l}{A}$$

$$\text{So, } A = \frac{p^2 \rho L}{w v^2 \cos^2 \phi}$$

$$Z_b = 3 A L$$

$$= 3 \frac{p^2 \rho L^2}{w v^2 \cos^2 \phi}$$

$$Z_b = 3 \frac{p^2 \rho L^2}{w v^2 \cos^2 \phi}$$

D''P

$$Z_b = 3 \frac{p^2 \rho L^2}{w v^2 \cos^2 \phi}$$

Kg jv#M|

2 | $D''P + fv + \ddot{e} + RU^a v \dot{Y}wgk b j v B + bi$

$\ddot{y}Zve, w \times ic \ddot{O}gvYt$

$$BbcyUcvIqvi = P + \dot{g}vUAcpq \text{ (jm)}$$

$$= P + \frac{p^2 \rho L}{v^2 \cos^2 \phi A}$$

$$g + bKwi, cwievnxikv + i > U + WbwmwU = J$$

$$Zvn + jA = \frac{I}{J} = \frac{p}{(\sqrt{3}v \cos \phi \cdot J)}$$

$$AZGeBbcyUcvIqvi = P \left(1 + \frac{\sqrt{3}JPL}{V \cos \phi} \right)$$

$$U^a v \dot{Y}wgk b \ddot{y}Zv = \frac{\text{Output power}}{\text{Input power}}$$

$$= \left(1 - \frac{\sqrt{3}JpL}{V \cos \phi} \right) |$$

GLvb + \dot{K} Avgiv + $\dot{L} + Z$ cvB + h, $D''P$

$\dot{f}v + \ddot{e} + RU^a v \dot{Y}wgk b j v B + bi \ddot{y}Zv + \dot{e}kxnq |$

mgvb cvIqvi +cÖi#Yi +ÿ#Î wWwm `yBZvi cxwZi
 Zzjbvq Gwm wZb#dR wZbZvi cxwZi Zzjbv Ki|

DËit Dfq+ÿ#Îmg `yi#Zi

cvIqvimg `ÿZvq+tcÖi#Yiwe#ePbvqcvIqviAcPqmgvb#e|

ÿZviwWwm+ÿ#Îg#bKwit

$$\begin{aligned}
 \hat{K}Uv \pm iG_{es} A_v \# _ \textcircled{i} \quad g \# a \cdot w_{eiv} R_{gvbme} \textcircled{v} w a K + f v \# \ddot{e} R &= V_m \\
 jvBbKv \# i \rangle U &= I_1 \\
 c\ddot{O}wZjvB \# bi \dagger iva &= R_1
 \end{aligned}$$

$$AZGe + gvUcvIqvip = V_m I_1$$

$$cvIqvijmW = 2I_1^2 R_1$$

wZb#dRwZbZviGwm+ÿ#Ît

$$c\ddot{O}wZ jvB \# bi \dagger iva = R_2$$

$$\begin{aligned}
 \#jvWd\ddot{v} \pm i &= \cos \emptyset \\
 jvBb Kv \# i \rangle U &= I_2 \\
 \#fv \# \ddot{e} \# R_{ir.m.s} G_{igvb} &= \frac{V_m}{\sqrt{2}}
 \end{aligned}$$

$$\begin{aligned} P &= 3V_p I_p \cos \phi \\ &= 3 \frac{V_m}{\sqrt{2}} I_2 \cos \phi \end{aligned}$$

$$P = 3I_2^2 R_2$$

$$V_m I_1 = 3 \frac{V_m}{\sqrt{2}} I_2 \cos \phi$$

$$I_1 = 3 \frac{I_2}{\sqrt{2}} \cos \phi \dots \dots \dots (1)$$

$$3I_2^2 R_2 = 2I_1^2 R_1$$

$$\frac{R_1}{R_2} = \frac{1}{3 \cos^2 \phi} = \frac{a_2}{a_1}$$

$$\frac{\text{Total volume of the three wire ac}}{\text{Total volume of the two wire dc}} = \frac{3}{2} \times \frac{1}{3 \cos^2 \phi} = 0.50.$$

1) $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$

$\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$

1) $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$ $\frac{3}{2} \sqrt{3} I_a \cos \phi$

$$\frac{\text{Total volume of the ac three phase four wire}}{\text{total volume of the dc two wire}} = \frac{3.5 a_2 L}{2 a_1 L}$$

$$\frac{3.5}{6 \cos \phi^2} = 0.5833 = 58.33\%$$

U^avÝwgkb I wWw ÷^aweDkb Gi Rb`Kvh©Kvix †fv‡ëR

U^avÝwgkb †fv‡ëR e,,w× †c‡i Zzjbvgyjk Kg AvqZ‡bi

KÛv±i †g‡Uwiqvj cÖ‡qvRb nq, d‡j KÛv±i LiP Kg c‡i|

ZvB me©wb‡œ KÛv±i K ÷ ivL‡Z †fv‡ëR‡K m‡œeZ

e,,w× Kiv nq|Avevi U^avÝwgkb †fv‡ëR e,,w× †c‡j,

Bbmy‡jUi, U^avÝdigvi, myBPwMqvi I Abvb`hš¿cvwZi

LiP AvbvcvwZK nv‡i †e‡o hvq| ZvB U^avÝwgkb †fv‡ëR

MÖnY‡hvM` mxgvq e,,w× Ki‡Z nq| me LiP

me©wb‡œ ch©v‡q ivL‡Z †h †fv‡ëR cÖ‡qvRb nq,

Zv‡K wgZeqx †fv‡ëR e‡j| GKUv ÷vÛvW© U^avÝwgkb

†fv‡ëRn ivL‡Z wb‡œv³ dv±i ,‡jv we‡ePbv Kiv

nq| U^avÝdigvi, myBPwMqvi, jvBwUwbs G‡i ÷vi Ges

Bbmy‡jUi mv‡cvU© BZvw`|

me©+cyvwgZeäxkUv±imvBRwbjfc+Y+Kjwf#bim~Îw

vjKz#jkbt

B#KvbwgKU^avÝwgb+fv#ëRKüjKz#jk#biRb^{..}

Kvejwimvm© nÛÛeyK KZ...©K

cÖ`ËGKwUm~ÎAb~m,,Znq| m~ÎwUwbæœifct

V = 5.5f $\sqrt{\frac{Lkm}{1.61} + \frac{Load\ in\ KVA}{150}}$ **Ky**

Uwee,,ZKiYtcÖkœt +Kjwf#biwgZeäxm~ÎwUwee,,Z
Kij

DËitkw³ cwien#bitÿ#Î #h cwievnxZv#iicÖ-'"Q#`
cÖv_wgKLi#Pievwl©K my` I AePq,
KÛv±i+iwR÷vÝRwbZevwl©KAePqK...Z Gbvwr© K#÷i
mgvbnq, D³ cÖ-'"Q#`B wgZeäxcÖ-'"Q`|
cwieZ©bkxjevwl©Kpvr© Tk PA Gesevwl©KAcPqRwbZPvr©

Tk^Q/_A nq , Zvn#j+Kjwf#bi

myÎbyhvqx , PA = ^Q/_A |

cOkœ t †Kjwf#bi wgZeqx m~IwU wee,,Z I
eüLü Ki|



DEit 1881 mv#j weÁvbx †Kjwfb B#KvbwgK KÛv±i
mvBR wbifc#bi Rb`GkwU m~Î cÖeZ©b K#ib, Zvnn
†Kjwf#bi m~Î bv#g cwiwPZ| Zvi g#Z U^avÝwgkb
juB#bi ewl©K LiP b~bZg ivL#Z †h cÖ`'#"Q#`i Zvi
eënnvi Kiv nq, Zvnn n#e me©#cÿv wgZeqx|
eüLüt eücK A#_© U^avÝwgkb juB#bi †gvU LiP `yB
As#k wef³t

1| gyja#bi Ici ewl©K PvR©

2| ewl©K kw³i AePqRwbZ LiP|

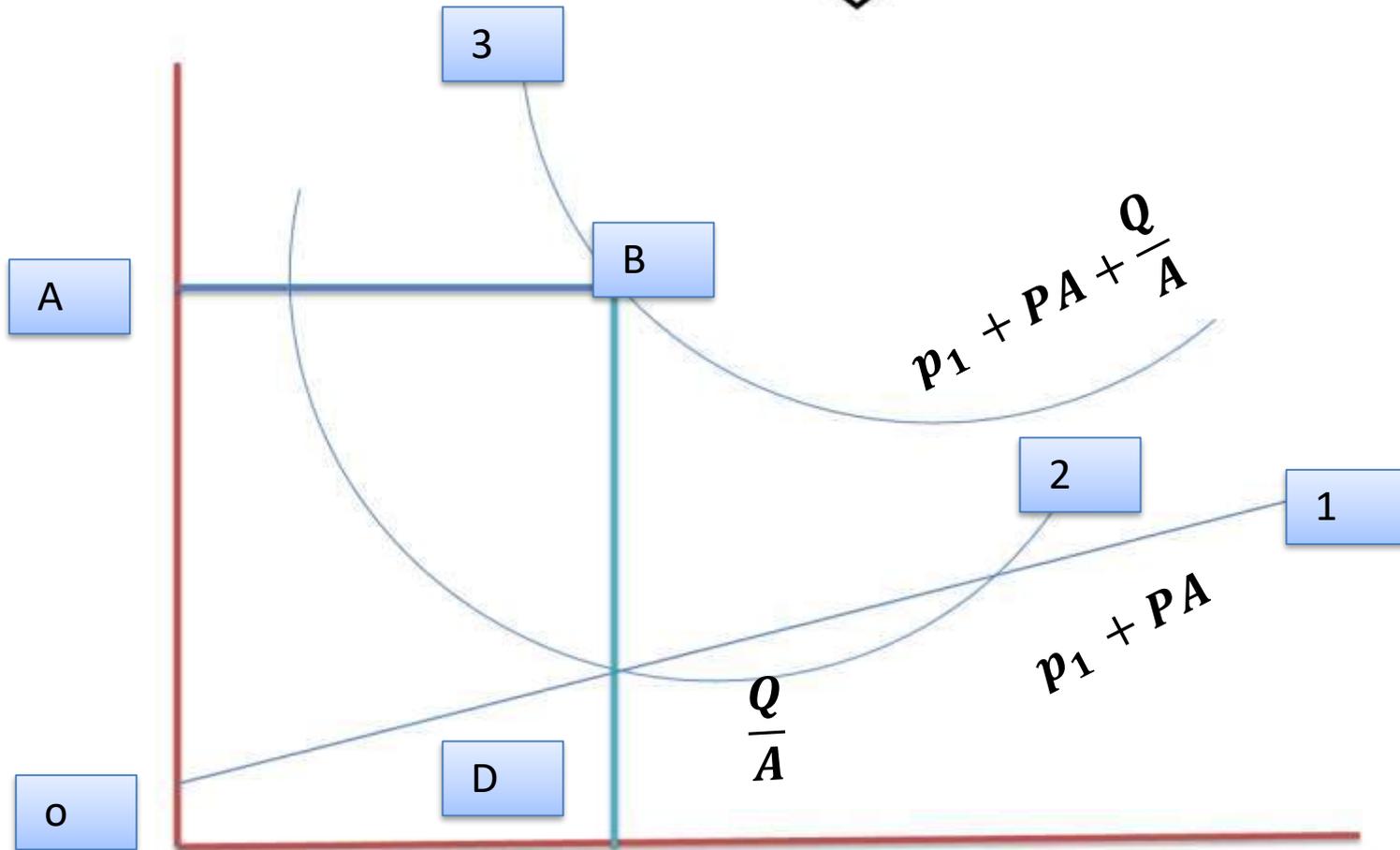


1 | $gyja\#biIciewwl\textcircled{C}KPvR\textcircled{C}tU^a v\acute{Y}wgkbjvB\#bi$
 $Bb\div\#jk\#bimvgwM\ddot{O}Ke\ddot{a} A_ \textcircled{C}vrK\hat{U}v\pm imv\#cvU\textcircled{C} I$
 $Bbmy\#jU\#ii \ `vg Geswbg\textcircled{C}vYe\ddot{a}BZ\ddot{u}w`$
 $Li\#Pievwl\textcircled{C}K m\sim ` I AePqgyj\ddot{I} AZGeevwl\textcircled{C}K m\sim `$
 $GesAePq = Tk(P_1 + PA) \dots (1)$



2 | $jevwl\textcircled{C}K kw\ddot{I} AePqRwbZLiP =$ $Tk \cdot \frac{Q}{A} GLv\#bQ a^a\ae|$
 $AZGeerm\#it\#gvUAvw_ \textcircled{C}K \ddot{y}wZL = [Tk(P_1 + PA) + Tk \cdot \frac{Q}{A}]$
 $GLb \frac{dL}{dA} = 0 \quad GB \ddot{y}wZicwigvbme\#P\#q \quad Kg \quad n\#e| \quad ZvB$
 $Dc\#iv^3 \quad mgxKib \quad \ddot{+}_ \#K \quad cvIqv hvq , \quad PA = \frac{Q}{A} |$

Graphical Representation of kelvin's law:



+KviwdWv#iimv#h

wK#jvIqvUcvIqvimieivnKi#Zn#e|

ms'vcbmncÖwZwgUviKve#ji `vg (6A+1.3)UvKv,

+hLv#bcÖwZKve#jicÖ-'#Q` A eM©#mw>UwgUvi |

evrmwiK m~` I AePq 10% AePqK...Z GbvwR©i `vg 5

cqmv cvi BDwbU| Zv#iiAv#cwÿKtiva1.75 × 10⁻⁶Ing-

#mwgn#jZv#iim#ev©"P B#Kv#bvwgKvjmvBR I

B#Kv#bvwgKvjKv#i>U#WbwmwUwbY©q Ki|

mgvavb t
+IqvAv#Q t

cÖwZwgUviKve#ji `vg TK. (6A+1.3) UvKv, 1000wgUvi

Kve#ji `vg = 1000 × TK. (6A+1.3)|

10% wnmv#eevwl©K m~` GesAePq =

$$\frac{10}{100} \times (6000A)Tk = Tk600A$$

$$\rho = 1.75 \times 10^{-6} \Omega - cm, A = ? \text{ And } \frac{I}{A} = ?$$

$$R/\text{km} = \frac{\rho l}{A} = \frac{1.75 \times 10^{-6} \times 1000}{A} = \frac{0.175}{A} \Omega$$

$$\text{Full load current } I = \frac{p}{V} = \frac{100 \times 1000}{500} = 200 \text{ amps}$$

$$\text{Energy loss } W = 2I^2 R t \times 10^{-3} \text{ KWH}$$

$$= 2 \times 200^2 \times \frac{0.175}{A} \times 8760 \times 10^{-3} = \frac{1.23 \times 10^5}{A} \text{ KWH}$$

Energy loss = 5 cqm vwnmv eAePqK...Z

$$\text{Energy loss } W = T_k \times 0.05$$

$$\times \frac{1.23 \times 10^5}{A} \text{ KWH} = T_k \frac{6150}{A}$$

$$\text{Energy loss } W = T_k \frac{6150}{A} = T_k 600A$$

$$A = 3.201 \text{ cm}^2$$

$$\text{Current density} = \frac{I}{A} = \frac{200}{3.201} = 62.96 \text{ amp/cm}^2.$$

Aaivq -2

wm#÷g j#mi aibmgyn

2.1 $wm^{\#} \div g \text{ jmt}$

$wm^{\#} \div g \text{ jm wK?}$

Drcv`b †K‡>`^ai wbR^{-^} eënvimn hš;cvwZi AcPq,
cwienbK...Z Zv‡ii †iwR÷v^Y RwbZ AcPq Ges Abvb`
KvwiMwi-AKvwiMwi AcPq `yiæb mvgwMÖKfv‡e †h
AcPq nq Zv‡K $wm^{\#} \div g \text{ jm e‡j|}$

$wm^{\#} \div g \text{ jm} = (\dagger gvU \text{ Drcvw`Z kw}^3 - \dagger gvU \text{ eëüZ}$
 $kw^3) / (\dagger gvU \text{ Drcvw`Z kw}^3)|$

$wm^{\#} \div g \text{ jm} \dagger K \text{ Av}_\text{©} \text{ mvgwRK } \dagger c\ddot{O}yvc\ddagger U \text{ c}\ddot{O}avbZ$
 $`yBfv\ddagger M \text{ fvM Kiv hvq t}$



KvwiMwi

AKvwiMwi|

1| KvwiMwi jmt K) cwienb jvB#bi InwgK

AePq,

L) eënvh© hš;cvwZi AcPq

M) B>UviKv#b#±W †bUIqv#K©i

AePq,

N) wdwWs eë⁻vcbvi AePq ,

O) we`yr †K#>`^ai wbR⁻^ eënv

RwbZ AePq GB j#mi AšÍ©fz³|

2| AKvwiMwi jmt K) A%_oea ms#hvMRwbZ

jm|

L) KbRvαúkb jm|

M) wewjs jm |

N) Kv#jKkb jm BZvüw`|

2.3 KwwiMwi jm Kgv#bvi Dcvqmgynt

1| Drcv`b †K>`a n#Z bó BDwbU, #jv hZ`ayZ
mæçe mwi#q †djv ev †givgZ Kiv|

2| ey÷vi U^avÝdigvi eënv#i K#i †fv#ëR
ti, #jU#ii gvb Dbœqb K#i|

3| †QvU #QvU cøv#>Ui gva#g -'vvbxq
Pvwn`v cyiæb Kiv|

4| †KejgvÎ wck AvIqv#i wK^α^v we#kl
cwiw-`wZ#Z MÖxW eënvvi Kiv|

5| MÖxW mve#÷k#b eëüZ U^avÝdigvi,
myBPwMqvi I Abvb`K#>U^avwjs BDwbU, #jv
cwieZ©b K#i|

AKvwiMwi jmmyn Kgv#bvi Dcvqt

**1| A%_oea we`yri ms#hvM Ly#R †ei Kiv Ges
aiv co#j wew"Qbœ Kiv|**

**2| A%_oea ms#hvMKvix#K K#Vvb AvB#bi
AvIZvq wb#q Avmv|**

**3| ÎæwUhy³ wgUvi cwieZ©b K#i ,bZzb
wgUvi ~'vcb Kiv|**

4| -^íZg mg#q e#Kqv wej Av`vq Kiv|

**5| cÖvkvmwbK AeKvVv#g_v#K †X#j
mvRv#bv|**

6| wbqwgZ wgUvi wiwWs gwbUwis Kiv |

2.4 cvIqvidv±iDbœqbt

Avgiv Rvwb, wK#jvIqvU =
†KwfG×cvIqvidv±i
ZvB Dc#iv³ mgxKib†_#K Avgiv†`L#Z
cvB#h, cvIqvidv±ihZ Kg n#e†KwfG†iwUs
ZZ †ekxn#e|
A_v©re,,nZAvKv#ii†gwkbccÖ#qvRbn#ehvn
vAZvšÍevqeûjnq |
myZivsmKjmyweaviK_vwe#ePbvK#icvIqvi
dv±iDbœqbKivwe#klcÖ#qvRb|

cvIqvi dv±i Dbœq#bi myweavmgynt

1|  †KwfG Gi gvb Kg nq , weavq †ewk cwigvb
wk#jvIqvU cvIqvi mieivn Kiv hvq|

2| jvB#b Kg Kv#i>U cÖevwnZ nq, d#j jvBb jm Kg nq
Ges U^avÝwgkb `ÿZv e,,w× cvq|

3| cwievnx Zvi,#jv wPKb AvK...wZi †ekx nIqvq Kcvi
†mwfs †ekx nq|

4| cv^aIqvi dv±i gvb hZ DbœZ n#e jvBb †i,#jkb ZZ
DbœZ n#e|

5| mvwe©Kfv#e %œe`yüZK †gwkb I hš¿vs#ki
ms⁻vcb, msiÿY I cwiPvjb LiP Kg nIqvq cÖwZ GKK

we`yř Drcv`b LiP Kg co#e|

BKzBc†g>U ,#jv eëüZ nqt



1| **D" P cvlqvi dv±i mœúbœ †gvUi t †hgb**
Kg#cb#m#UW BbWvKkb †gvUi ,wmb#&µvbm
†gvUi BZv̄w` cÖvq GKK cvlqvi dv±#i cwiPvwjZ
nq| ZvB Bnv#`i gva#g cvlqvi dv±i DbœZ nq|

2| **†dR GWfvÝvi t †dR GWfvÝvi †gvU#ii mwnZ**
eënv̄i Kiv n#j, D³ †dR & GWfvÝvi †_#K †ivUi
mvwK©#U cÖ#qvRbxq G·vBwUs Kv#i>U cvq, d#j
†gvUi A#cÿvK...Z DbœZ cvlqvi dv±#i cwiPvwjZ
nq|

3| **÷v̄wUK KücvwmUi t G c×wZ#Z wZbwU**
AvB#WbwUKvj KücvwmUi#K ÷vi ev †WjUv
ms#hvM K#i, jvB#bi mwnZ cÿivjv#j ms#hvM K#i
cvlqvi dv±i#K DbœZ Kiv nq|

4| Kücvwm#UÝ ey÷vi **t** G c×wZ#Z
cÖwZwU jvB#bi mwnZ KücvwmUi#K
U^avÝdigv#ii gva#g wmwI#R ms#hvM
K#i cvIqvi döv±#ii gvb DbœZ Kiv nq|

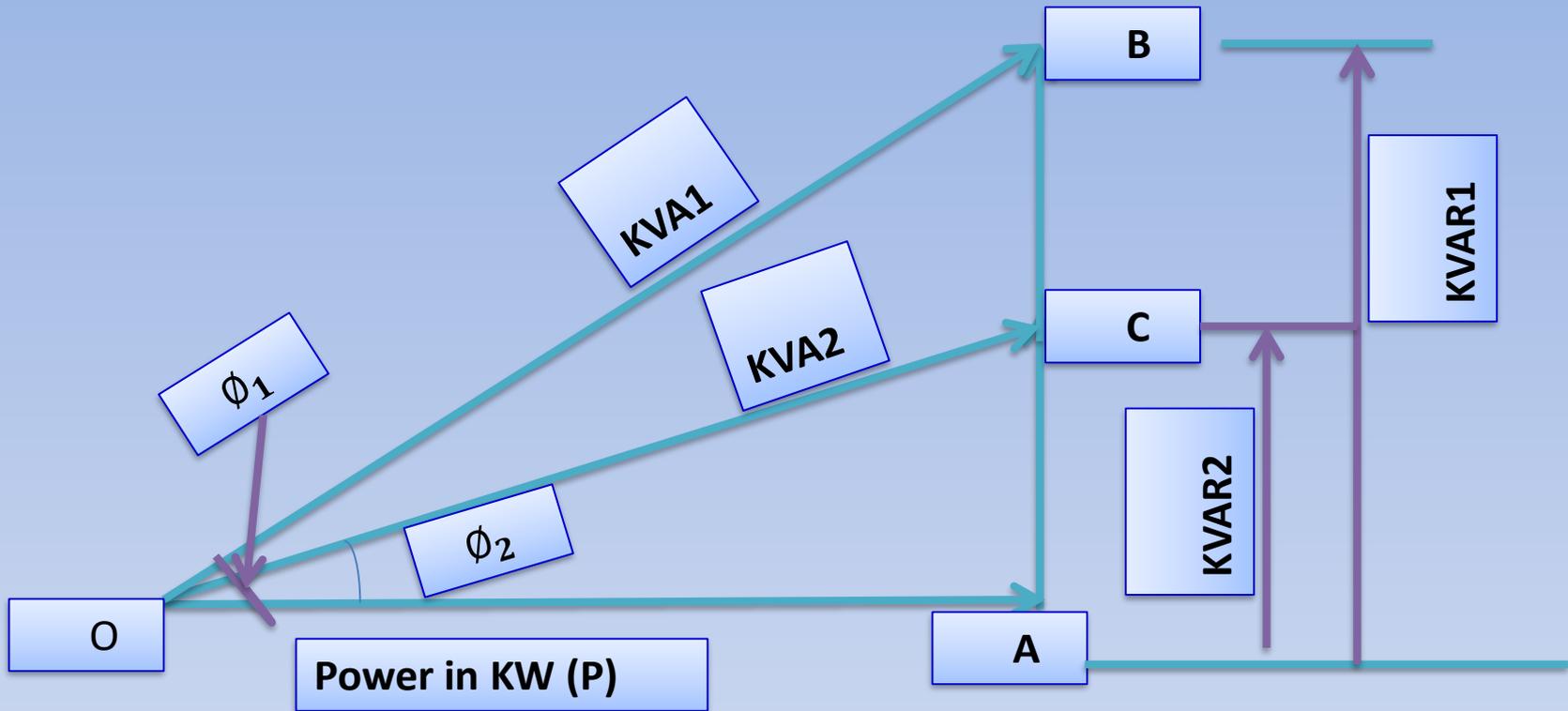
5| wmb#µvbvm K#ÛÝvi **t** hLb GKwU
Ifvi G·vB#UW wmb#µvbvm †gvUi#K
†jvWwenxb Ae⁻vq Pvjbv Kiv nq,ZLb
KücvwmU#ii bÿq GwU jvBb †_#K

wjwWs Kv#i>U †bq| G ai#bi Ifvi
G·vB#UW wmb#µvbvm †gvUi#K
wmb#µvbvm K#ÛÝvi e#j|

cÖkœt me©v#cjvAwakmvkÖqxcvIqvidv±#ii
mgxKibwUwbY©q Ki|

$$A_{ev} + \text{LvI} + h, \cos \emptyset_2 = \sqrt{1 - \left(\frac{y}{x}\right)^2} |$$

DËi t cvIqvidv±i#K+h
gv#bDbœZKi#jevrmwiKm#ev©"P mvkÖq N#U,D³
cvIqvidv±i#Km#ev©"P mvkÖqxcvIqvidv±ie#j|
cÖgvYtg#bKwi, GKRBMÖvnKcos ∅₁ cvIqvidv±#i P KW
wck+jvWMÖnbKi#QGesm#ev©"P Pwvn`viRb`
ZvievrmwiKPvR© avh© Kivn#q#QcÖwZ+KwfG#ZTK X
. cvIqvidv±i#KDbœZK#icos ∅₂ Kivnj| cvIqvii×Ki#biRb`
evrmwiKeqcÖwZwk#jvfvig TK y. n#jcvIqvi U^avBG#1/2j
+_#K cvB,



$$KVA1 = \frac{P}{\cos \phi_1} = P \sec \phi_1, \quad KVA2 = P \sec \phi_2$$

Economical Maximum demand Charge in a year

$$= Tk.X(KVA1-KVA2) = Tk.XP(\sec \phi_1 - \sec \phi_2) \dots (1)$$

KVAR Giwnmvet

$$KVAR1 = P \tan \phi_1, \quad KVAR2 = P \tan \phi_2$$

cvIqvidv±iKv#iKkbBKzBc#g>U KZ...©K mieivnK...Z wjwWs

$$KVAR = KVAR1 - KVAR2$$

$$= p(\tan \phi_1 - \tan \phi_2)$$

$$AZGecvIqvidv±iKv#iKkbBKzBc#g>UiRb^{\cdot}evl©wiKLiP =$$

$$TK. Py(\tan \phi_1 - \tan \phi_2) \dots (2)$$

$$AZGe^{\dagger}bUevwl©KmvkÖqS = Tk XP(\sec \phi_1 - \sec \phi_2) - TK.$$

$$Py(\tan \phi_1 - \tan \phi_2) \dots (3)$$

$$Dc^{\#}iv^3 \quad mgxKi^{\#}b^{\dagger}Kejgv\hat{I} \quad \phi_2 \quad cwieZ©bkxj|$$

$$AZGe^{\dagger}bUevwl©Kmvkqxn^{\#}e \frac{ds}{d\phi_2} = 0$$

$$\frac{ds}{d\phi_2} = y \sec \phi_2^2 - x \sec \phi_2 = 0$$

$$\cos \phi_2 = \sqrt{1 - \left(\frac{y}{x}\right)^2}$$

~~mgm~~ ~~bs~~ ~~1t~~ GKwU wkí cÖwZôv#b wZb#dR
400 †fvë 1500 wK#jvIqvU, 0.6 jvwMs cvIqvi
dÿ±#ii †jvW Av#Q| G cÖwZôv#b ÷vi c×wZ#Z
KücvwmUi eÿsK eÿnvi K#i cvIqvi dÿ±#ii gvb
0.8 jvwMs G DbœZ Ki#Z KücvwmU#ii gvb
wbY©q Ki|

#`IqvAv#Qt

$$P = 1500 \text{ Kw} \quad V = 400 \text{ volt ,}$$

$$\cos \phi_1 = 0.6 , \quad \phi_1 = \cos^{-1}(0.6) = 53.13^\circ$$

$$\cos \phi_2 = 0.8 , \quad \phi_2 = \cos^{-1}(0.8) = 36.86^\circ$$

mgvavbt

$$\text{KVAR} = 1500(\tan 53.13 - \tan 36.86)$$

$$= 875.39 \text{ kVAR}$$

$$\text{KücvwmUiVAR/ph} = \frac{875.39 \text{ kVAR}}{3} = 291.67 \text{ KVAR}$$

$$\div \text{vi ms\#hv\#MiRb} \cdot V_p = \frac{400}{\sqrt{3}} = 230.94 \text{ V}$$

$$\text{VAR/PH} = V_{plc} = V_p^2 \omega C$$

$$\text{Therefore, } C = \frac{\text{VAR/ph}}{V_p^2 \omega}$$

Aaÿq 3

Ifvi#nW jvBb mv#cvU©

Ifvi#nW jvB#bi gyj Dcvskmgy#ni bvgt

1| mv#cvU©t †cvj ev UvIqvi Gi D" PZv wbf©i
K#i jvB#bi Kvh©Kvix †fv#ë#Ri Dci |

2| μmAvg© I K¬vüαút ÷x#ii G#1/2j †mKkb hv
Kv#Vi Žix|

3| Bbmy#jUi: PxbvgvwU ev Møvm wbwg©Z|

4| KÛv±i

5| MvB #÷

6| jvBwUwbs G#i÷vi

7| wdDR ev AvB#mv#jwUs myBP

8| MvW© Iqvi

**jvBb mv#cv#U©i
cÖKvi#f`t**

**jvBb
mv#cvU©**

Kv#Vi †cvj

÷xj †cvj

KswµU

jvwUm ÷xj

cÖkœt GBP UvBc#cvj †Kv_vq eëüZ nq?

cÖkœt Wvœúvi I Rvœúvi Gi gv#S cv_©K`Kx?

cÖkœt †Kvb ai#bi †cv#j Uvbv eënyi Kiv nq?

cÖkœt wm#1/2j mvwK©U I Wvej mvwK©U ej#Z wK

eySvq? G#`i gvS Zzjbv Ki|

Aaÿq- 4
cwievnx Ges cwievwn c`v_©

~~4.1 Ifvi#nW U^avYwgkb I wWw÷^aweDkb jvB#b~~

eëüZ wewfbœ ai#bi KÛv±i t

1| Kcvi

2| Gÿjywgwbqvg

3| ÷xj †KviW Gÿjywgwbqvg|(G.wm.Gm.Avi)

4| MÿjfvbvBRW ÷xj KÛv±i|

1| Kcvi D" P Uvb mnb ÿgZv I ê`yÿZK cwievnxZvi

Kvi#b nvW©W^ab ÷^av#ÛW Kcvi DrK...ó cwievnx

wnmv#e we#ewPZ n#q#Q| Gi `yBwU myweav i#q#Q

,

1| Bnvi Kv#i>U †WbwmwU †ekx nIqvi Kvi#b

wPKb Zv#ii cÖ#qvRb nq,

2| Bnvi KÛv±i mvi#d#m evZv#mi Pvc Kg c#o|

2| Gÿjywgwbqvg t Kcv#ii Zzjbvq Gÿjywgwbqvg
`v#g m-Ív Ges IR#b nvjKv|KÛvw±wf Kcv#ii Zzjbvq
A#bK Kg| Bnvi Zvi ZzjbvgyjK †gvUv nq , d#j
evZv#mi Pvc †ewk c#o|

3| ÷xj †KviW Gÿjywgwbqvg|(G.wm.Gm.Avi)t
Aluminium conductor steel Re-inforcedment bv#g
cwiwPZ| Gÿjywgwbqv#i †UbmVBj †÷^as_ Kg nIqvq
müM e,,w× cvq| ZvB †ewk -úvb cwievwn jvB#bi
Rb¨Gjywgwbqvg †gv#UB Dc#hwwM b#n| G Rb¨Gi
†UbmVBj †÷^as_ evov#bvi Rb¨Gi †Kvi gÿ#Uwiqvj
wnmv#e MüjfvbvBRW ÷xj Iqvi eënyi Kiv nq|
Bnv#K `xN© -úvb cwienx jvB#b eënyi Kiv nq|

cÖkæt Ifvi#nW jvB#bi Rb"mvavibZ wK wK KÛv±i

eëüZ nq?

cÖkæt ACSR ej#Z wK eySvq?

cÖkæt nvB U^avÝwgkb jvB#b cwievwn wnmv#e

Gvjywgwbqvg Zvi eënyi Kiv nq †Kb?

cÖkæt nvB U^avÝwgkb jvB#b G.wm.Gm.Avi eënyi

Kiv nq †Kb?

cÖkæt G.wm.Gm.Avi Gi êwkó`wjL|

cÖkæt B" P Pv#ci U^avÝwgkb jvB#b G.wm.Gm.Avi

eënyi Kiv nq †Kb?

Aaÿq-5

jvBb BbmyjUi I Zv#`i êwkóïng~n

5.1 wewfbœ ai#bi Bbmy#jUi

- 1| wcb Bbmy#jUi
- 2| mvm#cbmb Bbmy#jUi
- 3| †÷^aBb Bbmy#jUi
- 4| kÿKj Bbmy#jUi
- 5| †cvó Bbmy#jUi
- 6| MvB- Bbmy#jUi

Bbmy#jUi Gi Dcv`vbmɡ~nt

- 1| PxbvgvwU
- 2| Møvm
- 3| w÷UvBU
- 4| cvB#i·

PxbvgvwU Bbmy#jUi

enj eëüZ GB Bbmy#jUi PvBbv †K¬i mwnZ
cøvw÷K †Kiwjb, †djmcvi I †KvqvU©R cvIWvi
wgwk#q GKwU wbqwsŷZ ZvcgvÎvq %oZix Kiv
nq| Kg Zv#c G ai#bi Bbmy#jUi Zix Ki#j Zvi hvwsŷK
,Yv,Y e,,wx cvq| GB UvBc Bbmy#jU#ii
WvBB#jKwU^aK †÷^as_ 60 †Kwf/#mwg|
Møvm Bbmy#jUit Møvm Bbmy#jUi PxbvgvwUi
Bbmy#jUi A#cÿv `v#g m´Ív| cÖ#qvRbxq ZvcgvÎv
wbqŷY I cÖ#j#ci gva#g Gi `,,pZv, WvB-B#jKwU^aK
†÷^as_ I Av#cwyK †iva evov#bv hvq| Z#e Bnvi Pvc
mnb ÿgZv †ekx|
w÷UvBU Bbmy#jUit güM#bwmqvg wmwj#K#Ui
mwnZ wewfbø Abycv#Z güM#bwmqvg A·vBW I
wmwjKv wgwkÖZ n#g cÖK...wZBMZfv#e
w÷UvB#Ui DrcwË nq|

cvB#i·t we#kl cÖwμqvq cÖ`ZK...Z cvB#i· GK
cÖKvi KvPu,

hv Bbmy#jwUs †gwUwivqj wnmv#e eëüZ nq|
Gi WvB-B#jKwU^aK †÷^as_ Kg nIqvq G,#jv
myavibZ 11 †Kwfi Dc#i eënyi Kiv hvqbv|

5.3 Bbmy#jU †gwUwivq#ji MYV, Yt

1| Zv#ii Uvb I IRb mBevigZ h#_ó gReyZ nIqv `iKvi|

2| D`P WvB-B#jKwU^aK †÷^as_ cÖ`v#bi Rb`Gi wi#jwUf
cviw gwUwfwU †ewk _vK#Z n#e|

3| wj#KR Kv#i>U cÖwZnZ Ki#Z Gi tiwR÷vÝ †ewk
_vK#Z n#e|

4| cvsPvi †fv#ëR d¬vm Ifvi †fv#ëR †iwkI mαϕve`†ewk
_vK#Z n#e|

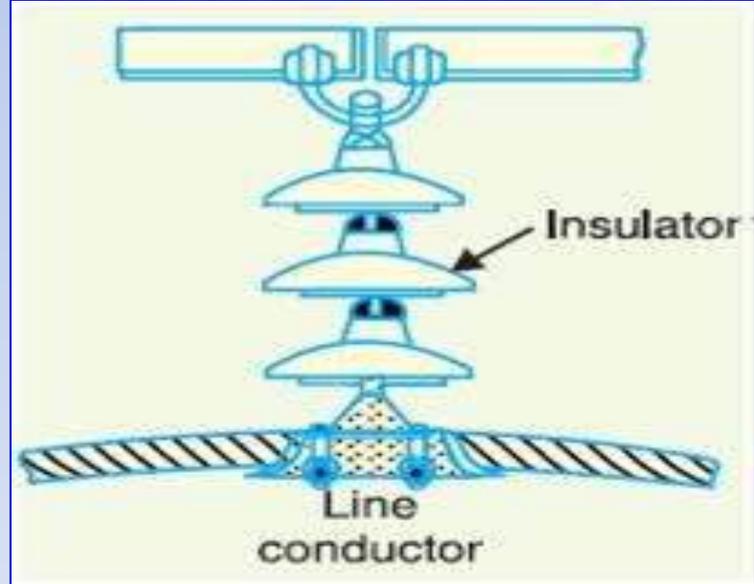
5.5 wcbUvBc Bbmy#jU#ii eY©bvt

wbœPv#ci jvB#b Uvb#R>U I Aí wePzwwZ#Kv#Yi
Gv#1/2#j †cvj,#jv#Z wcbUvBc Bbmy#jUi eënyi Kiv nq|
GwU wPbvgvwUi I big B-úv#Zi mgš^#q MwVZ| GB
Bbmy#jU#ii †mj,#jv 11 †Kwfi Dc#hvMx K#i Zix Kiv
nq| m#ev©"P 33 †Kwfi jvB#b wcb Bbmy#jUi eëüZ
nal



mvm#cbkb UvBc Bbmy#jUit

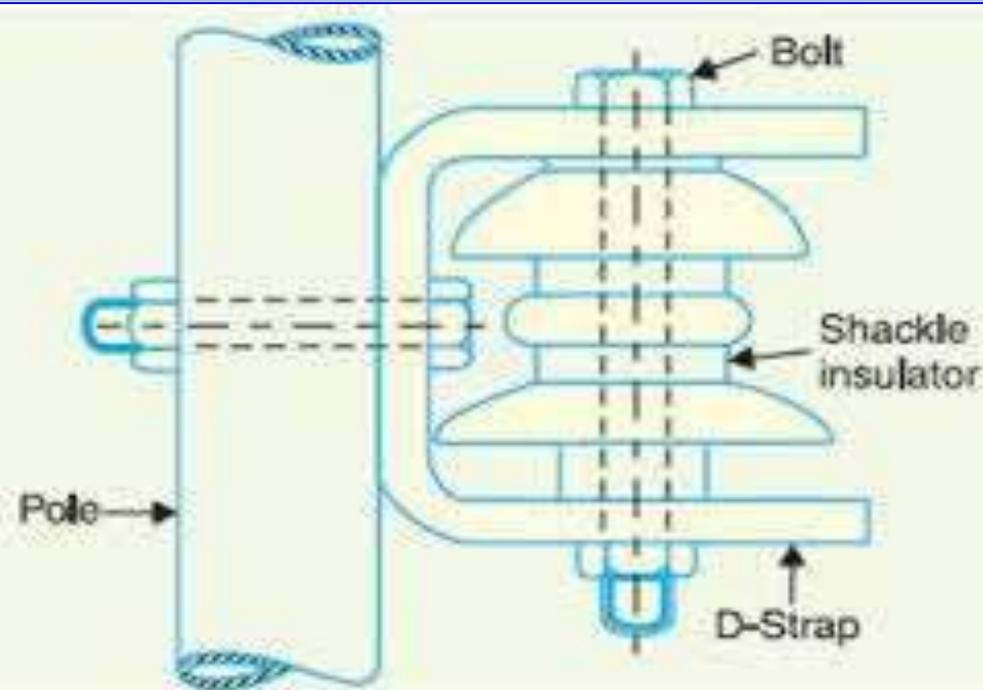
juB#bi +fv#eR 33 +Kwfi AwaK n#j juB#b GKvwaK
wW< m^wZ mvm#cbkb Bbmy#jUi eenvi Ki#Z nq|
cOwZwU wW< 11 +Kwfi Rb%oZix Kiv nq| wjsK
wK-c, PKP#K wPbvgvwUi wW< +gUvj Kvc BZw`i
m^#a MwVZ BbmjUi 230 +Kwf ivB#b eeuZ nal



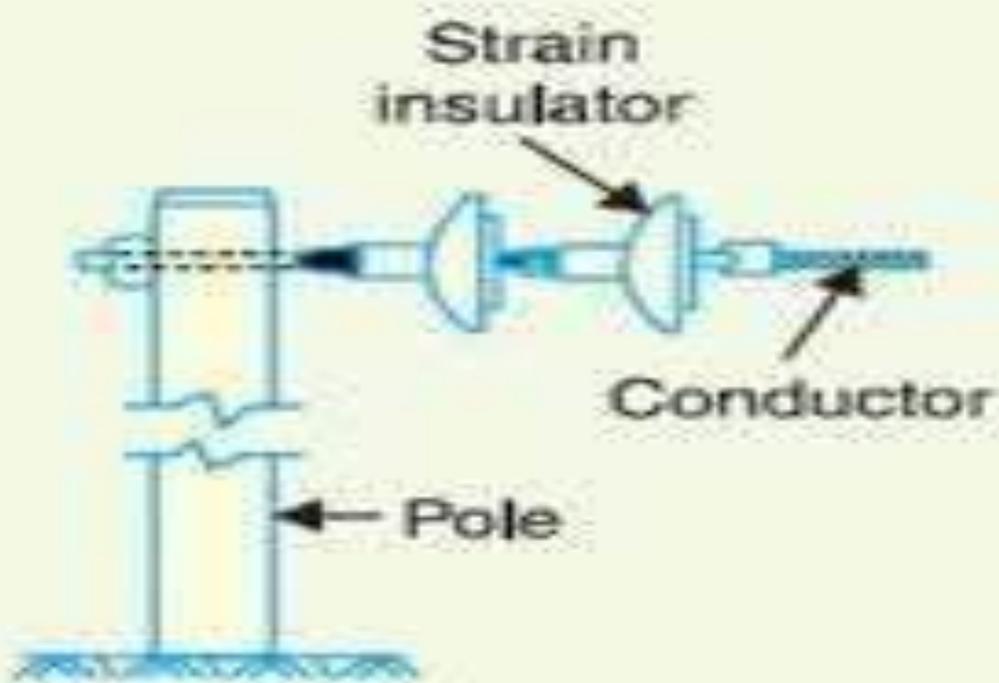
cÖkœt mvm#cbUvBc I wcbUvBc

Bbmy#jU#ii g#a"cv_©K"wjL

küKj Bbmy#jUit küKj ev ~úyj UvBc Bbmy#jUi GjwU
400/230 †fvë jvB#bi Uvwg©bv#j †ewk wePzÿZ
†Kv#bi Gv



‡ ÷^a Bb Bbmy ‡ jUi D" P Pvc jvB ‡ b, Uvwg ©bvj,
†mKkb Ges †KŠwYK †cvj UvIqv ‡i †hLv ‡b †ij
μwms ,nvBI ‡q I †ewk Uv ‡bi †j ‡Î GB Bbmy ‡ jUi
eēnvi Kiv nal



†cvó Bbmy†jUit AvDU†Wvi mve-†÷k†b GBP wU
evm evi, wWmKv†bw±s myBP BZw`i mv†cvwU©s
wnmv†e †cvó Bbmy†jUit



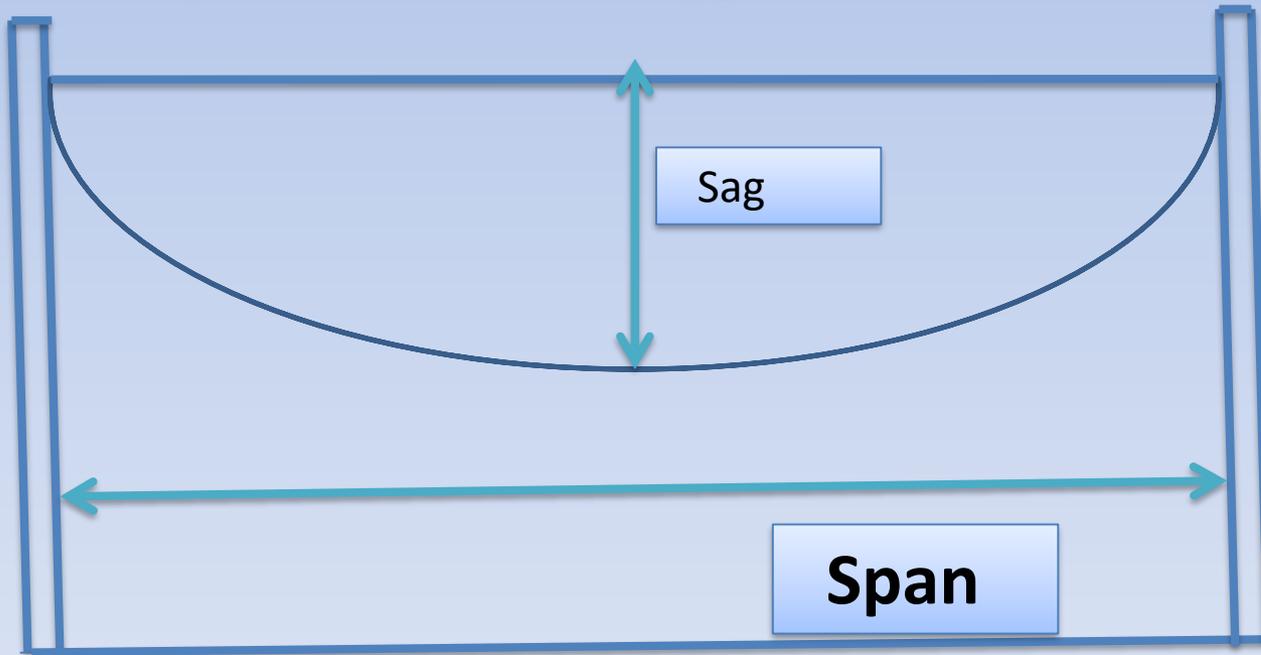
MvB- Bbmy†jUit
Ifvi†nW jvB†bi Mv



my†jUi

Aaüq- 6
mü≠Mi cÖfve

6.1 cwienb jvB#b m#Mt `yBwU †cv#ji g#a` Zvi
Uv^{1/2}v#bv n#j ZviwU wKQzUv Sz#j c#o| †cvj `yBwU
†h we>`y#Z Szjv#bv n#q#Q †mB we>`yØq w`#q
KvíwbK †iLv Uvb#j , D³ †iLv †_#K m#ev©"P Szjv#bv
we>`y ch©šÍ `yiZj#K m#M e#j|



*স্যাগের আনুমানিক হিসাবঃ (প্রশ্নঃ দেখাও যে সমউচ্চতায় দুটি পোলের মাঝে

পরিবাহির বুল $S = \frac{wl^2}{8T}$)

নিম্নের চিত্র অনুযায়ী, **OP** অংশে ক্রিয়াশীল দুইটি বাহ্যিক বল

১। একটি টেনশন **T** এবং অপরটি ২। **OP** অংশের তারের ওজন **W.X**,

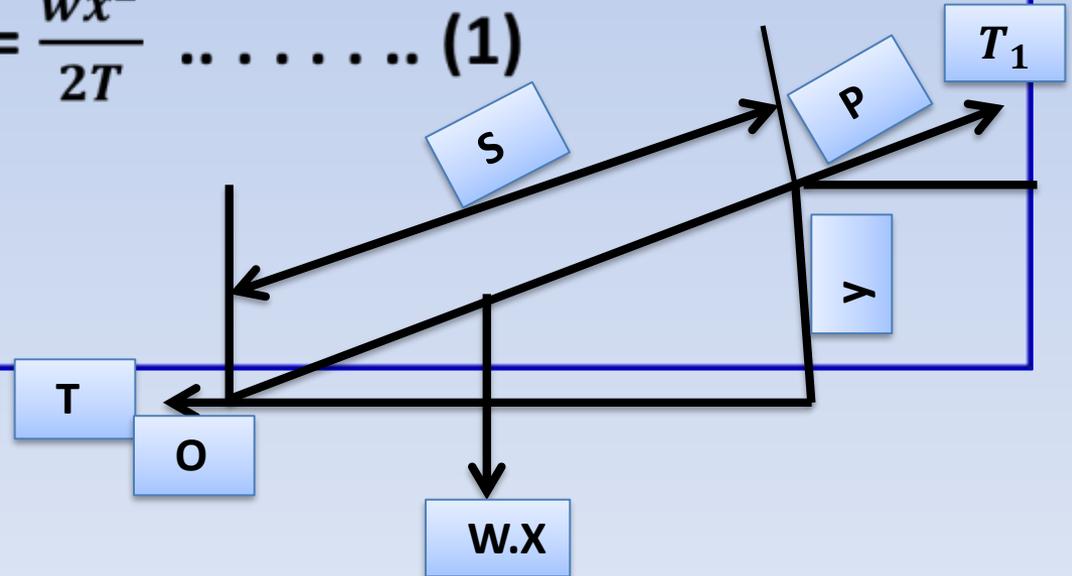
যা **O** বিন্দু হতে $\frac{X}{2}$ দূরত্বে উলম্ব নীচের দিকে ক্রিয়ারত। সুতরাং এই দুই

বলের জন্য **P** বিন্দুতে মোমেন্ট নিলে,

$$Ty = W.X. \frac{X}{2} = \frac{wx^2}{2}, \text{ so } y = \frac{wx^2}{2T} \dots \dots \dots (1)$$

$$\text{But } Y=S, X=L = \frac{l}{2}$$

$$\text{So sag}(S) = \frac{wl^2}{8T}$$



6.5 $m \cdot v = M \cdot v$

(hLbcwievwniDci

+KejS#oicÖfveKvRK#i)t

$g \cdot b \cdot K \cdot w_i$, $Z \cdot v \cdot i \cdot e \cdot v \cdot m$ = D m

GescÖwZwgUviZv#ii+gvUIRb = W kg.

cÖwZwgUviZv#iiwbR⁻ ^ IRb = W_c kg

cÖwZwgUviZv#iiewn⁻

+ÿÎd#jiDcievZv#miAvbyf,wgKPvc = W_w kg/M²

W_w = cÖwZwgUviZv#iicÖ#R#±W

GwiqvgvwëcøvBcÖwZeM©wgUv#ievZv#miPvc|

AZGe ,W= $\sqrt{W_c^2 + W_w^2}$

hw⁻ üvbl nq , Z#em#ev©"P Szjn#esag(S) = $\frac{wl^2}{8T}$

Dj^α ^ m·v·M·n#e = Scos θ

wµqvK#it

cÖwZ GKK ~#N©" +UvUvjKÛv±#ii I#qU,

$$W_t = \sqrt{((W + w_i)^2) + (W_w)^2}$$

W = Weight of conductor per unit length

= conductor material density × volume per unit length

Zv#iiev#m = d metre Gesei#diw_K#bm = t m nq

Zvn#jeidcovi ci Zv#ii me©#gvUe#m=(d+2t) metre

$$cÖwZwgUviZv#iicÖ#R#±W Gwiqv = [(d+2t) \times 1] m^2$$

$$eidmnZv#ii me©#gvU+ÿÎdj = \left[\frac{\pi}{4} (d + 2t)^2 \right] m^2$$

$$Zv#ii+ÿÎdj = \frac{\pi}{4} d^2$$

$$AZGeei#di+gvU+ÿÎdj = \frac{\pi}{4} [(d + 2t)^2 - d^2] m^2$$

$$ei#diAvqZb = \frac{\pi}{4} [(d + 2t)^2 - d^2] \times 1 m^3$$

$$\begin{aligned}
 W_i &= \text{Weight of ice per unit length} \\
 &= \text{density of ice} \times \text{volume of ice per unit length} \\
 &= \text{density of ice} \times \frac{\pi}{4} [(d + 2t)^2 - d^2] \times 1 \\
 &= \text{density of ice} \times \pi t (d + t),
 \end{aligned}$$

$$W_w = \text{wind pressure} \times \text{projected area}$$

$$\text{sag}(S) = \frac{Wl^2}{8T}, \quad T = \frac{\text{breaking stress} \times \text{area}}{\text{safety factor}}$$

$$Dj \alpha \wedge m \ddot{v} M n \neq e = S \cos \theta$$

$1 | 30 \text{ wgUvi } D''PZv \text{ wewkó''mgD''PZvi } \text{`yB UvIqv\#ii}$
 $g\#a\ddot{e}Z\text{©x Avbyf,wgK } \text{`yiZi } 250 \text{ wgUvi} | \text{ cwievwni}$
 $c\ddot{O}\text{''\#''Q` } 1.24 \text{ eM}\text{©}\#mw>UwgUvi, \text{ IRb } 1170$
 $\dagger KwR/wK.wg \text{ Ges } \dagger e^a wKs \dagger \div^a s_ \text{ 4218 } \dagger KwR/$
 $eM\text{©}\#m,wg | \text{ hw` } \dagger mdwU \text{ d}\ddot{v}\pm i \text{ 5 nq, } g\#a\ddot{w}e>\text{`y}\#Z$

~~$\#IgvAv\#Qt$~~
 ~~$cwievwni \dagger, wg \dagger \#K KZ Dc\#i \text{ vK}\#e?$~~
 $W_c/m = 1.170 \#KwR , l = 250 \bar{w}gUvi , \dagger e^a wKs \dagger \div^a s_ = 4218$
 $\dagger KwR/e.\#mw>UwgUvi, h = 30 \text{ wgUvi ,}$
 $A = 1.24 \text{ e.\#mw>UwgUvi , } M\ddot{O}vD\hat{U}wK \neg qv\#i\acute{Y} = ?$
 $mgvavbt$
 $T = \frac{4218 \times 1.24}{5} = 1046 \#KwR , Avbf,wgK m\ddot{v}M = \frac{1.17 \times 250^2}{8 \times 1046} = 8.73$
 m
 $\text{Vertical sag} = 8.73 \text{ m } [Wc=W]$
 $\text{So ground clearance} = 30 - 8.73 = 21.27 \text{ m}$

অধ্যায় ৭
ট্রান্সমিসন/ডিস্ট্রিবিউশন
লাইন জরিপ

ট্রান্সমিসন/ডিস্ট্রিবিউশন লাইন ডারিপের জন্য
প্রয়োজনীয় সার্ভে ইন্সট্রুমেন্টের তালিকা:

১। চেইন

২। তির

৩। কাঠের গজা

৪। রেঞ্জিং রড

৫। মেজারিং টেপ।

➔ রেঞ্জিং রডের কাজ কি?

Ans. কোন লাইনকে প্রসারিত করার কাজে কিংবা
কোন $\# \div kb \#K$ ভালভাবে চিহ্নিত করার কাজে

ব্যবহৃত হয়।

➔ থিওডোলাইটের ত্রুটিসমূহ কি কি?

➤ ইন্সট্রুমেন্ট সংস্থাপনে ত্রুটি

➤ ইন্সট্রুমেন্ট সমতলকরনে ত্রুটি

➤ প্যারালাক্স ত্রুটি।

cÖkœtলেভেলিং কাকে বলে?

#h Kjv#K%okj ev cÖwµqvi gva#g fz-c,,#ô wewfbœ

বস্তু বা বিন্দুর,Av#cwÿK অবস্থান,উচ্চতা,গভিরতা ইত্যাদি

নির্নয়ের কলা কৌশল ও প্রক্রিয়া আলচনা করা হয়,সে শাখাকে

লেভেলিং বলে।

➔ থিওডলাইট দিয়ে কি কি কাজ করা যায়?

১. স্যাগ নির্ণয়ের কাজে

২. আনুভূমিক কোণ মাপার জন্য

৩. উলম্ব কোণ মাপার জন্য

৪. দূরের বস্তু দেখার জন্য

৫. লেভেলিং এর কাজে

৬. কোন রেখার উপর বিন্দু স্থাপন, জরিপ রেখার

প্রসারণ, উচ্চতার তারতম্য নির্ণয়ের ক্ষেত্রে।

অধ্যায় ৮

VOLTAGE DISTRIBUTION OF SUSPENSION INSULATOR

স্ট্রিং দক্ষতা কি?

$$\% \eta = \frac{\text{Total voltage across the disc}}{N \times \text{Voltage across the disc nearest to the Conductor}} \times 100$$

➔ $V_3 = V_1(1+3K+K^2)$?

মনে করি শান্ট ও মিউচুয়াল ক্যাপাসিটেন্স এর অনুপাত,

$$K = \frac{C_1}{C}, C_1 = KC$$

লাইনের ভোল্টেজগুলো V_1, V_2, V_3 এবং লাইন ও আর্থের

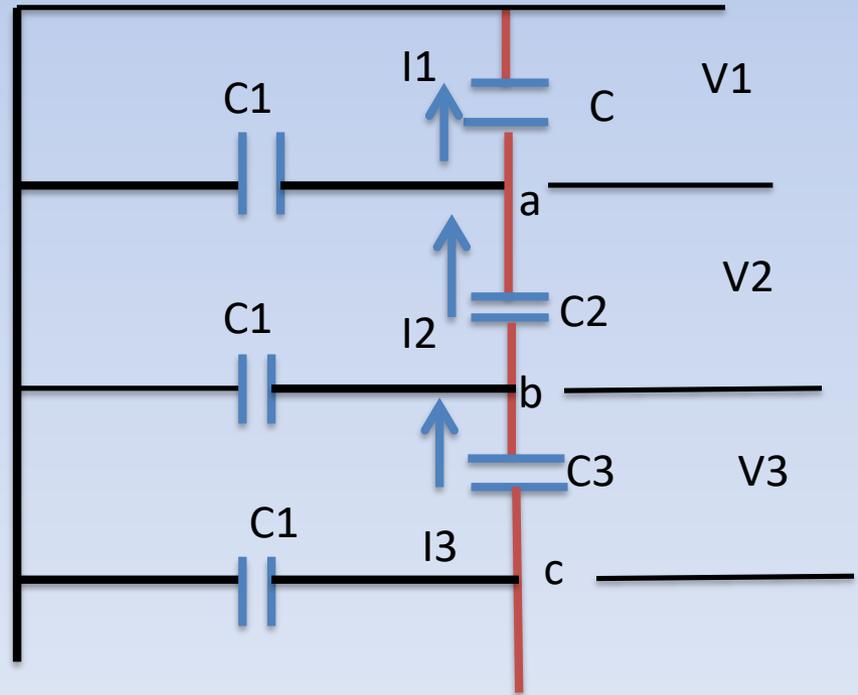
মধ্যে ভোল্টেজ = V

A বিন্দুতে KCL প্রয়োগ করে

$$I_2 = I_1 + I_a$$

$$\omega C V_2 = \omega C V_1 + \omega C_1 V_1$$

$$V_2 = V_1(1+K)$$



bবিন্দুতে KCL প্রয়োগ করে

$$I_3 = I_2 + I_b$$

$$\omega C V_3 = \omega C V_2 + \omega C k (V_1 + V_2)$$

$$\omega C V_3 = \omega C V_1 (1 + K) + \omega C V_1 K (1 + K) + \omega C K V_1$$

$$= \omega C V_1 (1 + K + K^2 + K + K)$$

$$= \omega C V_1 (1 + 3K + K^2)$$

$$V_3 = V_1 (1 + 3K + K^2)$$

গার্ড রিং পদ্ধতি:

এধরণের সংযোগে স্ট্রিং এর সকল ইউনিটে মিউচুয়াল ক্যাপাসিটেন্স এর মান সমান হয়। ফলে প্রত্যেক ইউনিটে একই পরিমাণ চার্জিং কারেন্ট প্রবাহিত হয়। চার ইউনিটের একটি ইন্সুলেটর স্ট্রিং বিবেচনা করি। ধরি প্রতি ইউনিটে মিউচুয়াল ক্যাপাসিটেন্স c এবং ভোল্টেজ v

A বিন্দুতে বিবেচনা করি,

$$I + I_x = I + i_1$$

$$I_x = i_1$$

$$3\omega C_x V = \omega m C V$$

$$C_x = mC/3$$

Aaüq -09
K#ivbv msNUb

9.1 Ifvi#nW U^avÝwgkb jvB#b

ev#mi Zzjbvq †ewk)
K#ivbv Avwo#Z Gwm mvcøvB cÖ#qvM c~e©K ax#i
ax#i evov#bv n#j Ggb GK ch©vq Av#m, hLb
†fv#ëR wbw`©ó`mxgv AwZµg K#i, G#K wµwU#Kj
wWmivcwUf †fv#ëR e#j|
G mgq KÛv±#ii Pvicv#k!© evZvm Av#qvbvBRW
nq Ges KÛv±#ii Pviw`#K wnm wnm kã K#i GKwU
&Clr Aby^{3/4}ij †e,bx Avfv wWmPvR© n#Z †`Lv hvq,
G#K K#ivbv wWmPvR© e#j| K#ivbv msNV#bi `iæb
ÿwZKi IRb Mÿm, cvIqvi jm, Ges †iwWI B>Uvidv#iÝ
D™¢e nq|

KmwwgK iwkw¥, AwZ#e, bx iwkw¥i wewKiY
Ges tiwWI AÜKwUwfwU Dcw'wZi
Kvi#b

me`©v evZvm wKQz Av#qvwbZ nq,
Kv#RB ^vfwweK Ae'vq KÛv±#ii PZzl
cvk!©Zi Av#qvbbvBRW evqy KYv gy³
B#jKU^ab cwRwUf Avqb I wbDU^avj
gwjwKDj Gi Aw'ÍZ; AYzfe Kiv hvq| hLb
KÛv±i`!#q +fv#ëR cÖ#qvM Kiv nq,ZLb
evqy gva#g c#Ubwkqvj MÖvwW#q>U
DrcwË nq| KÛv±i mvi#d#m Gi gvb
m#ev©"P nq|

GB c#Ubwkqvj MÖvwW#q>U Gi Rb·
B#jKU^ab MwZcÖvß nq| Av#ivwcZ †fv#ëR
hZ †tekx n#e,c#Ubwkqvj MÖvwW#q>U ZZ
†tekx n#e Ges B#jKU^abGi MwZ#eM ZZ
†tekx n#e& | hLb c#Ubwkqvj
MÖvwW#q>U Gi gvb hLb 30†Kwf/#mwg
nq ZLb gy³ B#jKU^ab,#jv h#_ó MwZ kw³
AR©b K#i | d#j GKwU wbDU^avj
g#jwKDj#K AvNvZ Ki#j Zv †_#K GK ev
GKvwaK B#jKU^ab wew"Qbœ n#q hvq|
Gfv#e gy³ B#jKU^a#bi msLv e,,w× †c#Z
v#K Ges wbDU^avj g#jwKD#ji mv#
msNI© NwU#q bZzb Avqb m,,wó K#i|&

9.2 K#ivbvi cÖfv#e jvBb

Zv#ii Dci †h mg^í wμqv cÖwZwμqv nq, Zvnn
wb#æ cÖ`Ë njt

1| KÛv±#ii Pvicv#k|© †e,bx Avfv cwijwÿZ nq|

2| GwU wnwms kã Drcbæ K#i|

3| K#ivbvi Rb`GKwU wbw`©ó`cwigvb cvIqvi
AcPq nq|

4| K#ivbvi Rb`DTM¢e IRb Mvm jvBb Zv#ii
mwnZ wewμqv K#i d#j Zvi ÿqcÖvß nq|

5| K#ivbv nvi#gvwBK Kv#i>U m,,wó K#i|

9.3 K#ivbvi Dci cÖfve we ÍviKvixmgynt

1| AvenvIqv gÛjt AvenvIqvi cvwicvwk!©K
Ae⁻'vi Dci K#ivbv wbf©ikxj| wkjve,,wói mgq
KYv, #jv AvqwbZ nq, weavq G mgq ZzjbvgyjK
Kg †fv#ë#R K#ivbvi DrcwË nq|

2| KÛv±i mvBRt KÛv±i mvBR , AvK...wZ Ges
mvi#dm KwÛk#bi Dci wbf©i K#i K#ivbvi
DrcwË nq| A#cÿvK...Z †gvUv Zvi n#j Kg nq|

3| KÛv±#ii cvi®úvwiK eëavbt KÛv±#ii eÿm
A#cÿv †⁻úwms Kg n#j K#ivbv msNwVZ nq|
†⁻úwms †ewk n#j B#jK#U^av#÷wUK †÷^am K#g

hvq d#j K#ivbv msNwVZ bvI NU#Z cv#i|
jvBb †fv#ëRt jvBb †fv#ëR Kg n#j K#ivbv
msNwVZ nq|

K#ivbvi myweav I Amyweavmg~nt

myweavt 1| K#ivbvi Kvi#b KÛv±#ii Pvicv#k!©
evZvm cwievwn#Z cwiwbZ nIqvq KÛv±#ii eÿm
AvbycvwZKnv#i †e#o hvq

2| GwU jvBwUwbs I Abÿb¨ Kvi#b m,,ó
U^avbwR#q>U#K Kwg#q Av#b|

Amyweavt

1| K#ivbvi Kvi#b cvIqvi jm nq, hv U^avÝwgkb `ÿZv#K
cÖfvweZ K#i|

2| K#ivbvi Rb¨IRb Mÿ#mi m,,wó nq| d#j avZe As#ki
ÿqcÖvß nq|

3| evmev#ii Rb`K#ivbv we#kl ÿwZKi|

4| K#ivbv wWmPv#R©i Rb¨ evmevi GjvKvq

myBPwMqv#ii Askmg~#ni ÿwZ nq|

wWmivcwUf wμwUKvj+fv#ëRt me©wbgæ+h

#dRUzwbDU^avj

+fv#ë#RK#ivbvmsNwVZnqZv#KwWmivcwUfwμwU

Kvj+fv#ëRe#j| G#K V_c ØvivcÖKvkKivnq|

$$V_c = \frac{V}{r \log_e \frac{D}{r}} \text{ Volt/cm}$$

wfRyqvj wμwUKvj+fv#ëR t

me©wbgæ+h #dRUzwbDU^avj +fv#ë#RjvBbKÛv±#ii

PZzwZ©#K ClrAvfv „këvbn#q I#V,

Zv#KwfRyqvjwμwUKvjwWmivcwUf+fv#ëRe#j|

GigvbwWmivcwUfwμwUKvj +fv#ëRA#cÿv+ekx|

$$V_v = m_v g_0 \delta_r \left(1 + \frac{0.3}{r\sqrt{\delta}}\right) \log_e \frac{D}{r} \text{ KV/phase}$$

K#ivbv jm Kgv#bvi Dcvqt

1| KÛv±i mvBR e,,w× K#i& |

2| KÛv±i †´úwms e,,w× K#i&

অধ্যায় ১০

ERACTION OF POLES/TOWERS AND DRAWING OF
OVERHEAD LINE CONDUCTOR

ট্রান্সমিসন/ডিস্ট্রিবিউশন লাইনে যেসকল পোল eëüZ হয় সেগুলো হল:

১.কাঠের পোল

২.স্টীল পোল

৩.কংক্রীট পোল

সেকশন পদ্ধতি:

সেকশন পদ্ধতিতে কতগুলো সুবিধা মত দৈঘ্যের টাওয়ারের প্যানেল সংযজন করে সম্পূর্ণ টাওয়ার তৈরি করা হয়।সুবিধা মত দৈঘ্যের দুটি টাওয়ারের পাসাপাসি বসান হয়।গিন পোল দার করান হয়।প্যানালের মাথাই ষ্টীলের দরি বাধা হয়।

➔ গিন পোল পদ্ধতি

- গিন পোল পদ্ধতিতে অল্প কয়েক জন লোকের দ্বারা ব০ ধরনের পোল গর্ত করে স্থাপন করা হয়। গিন পোলকে কতগুলো লাইন রসির সাহায্যে উল্লম্বভাবে খারা করা হয়। হুকে স্লিং দ্বারা পোলকে জরান হয়। যখন পোলটি বেশ উঁচুতে উঠে তখন পোলের গোঁড়াকে কাত করে গর্তের মধ্যে ঢুকানো হয়।



†iwR÷vŸ

Aaüq-11
jvBb cwiewwni

U^avÝwgkb jvB#bi jvBb a^ayeK

U^a  wgkb jvB#bi mg Í %o`N©`eivei
me©ÎK#ZK, #jv a^aæeK mgfv#e we Í...Z _v#K ,
GB a^aæeK, #jv#K jvBb ay^aeK e#j|
ay^aeK, #jv nj ,
1| †iwR÷vÝ
2| BÛvK#UÝ
3| Kÿcvwm#UÝ
U^avÝwgkb jvB#bi A#bK Kvh©µg GB a^aye#Ki
Dci wbf©i K#i|

cÖkoet cwievwni tiv#aimvaviYm~ÎwUwee,,Z Ki|
DËit+iwR÷vÿcwievwni GK we#klag©, th a#g©iRb·
Kv#i>UcÖev#ni c#_ evavm,,wónq| L %o`N©i
GKwUmylgcwievwnZv#iicÖ-`#”Q` A, so R= $\frac{\rho L}{A}$ n#e|

cÖkœ t jvBb a^ayeK ej#Z wK eySvq?
cÖkoet jvBb Kb÷vÛ ,#jvi bvg I GKK
wjL|
cÖkoet jyc#iwR÷vÿ ej#Z wK
eySvq?

Aaüq-12

U^avÝwgkb jvB#bi w⁻<b G#d±

GKwU KŪv±#ii g#a`w`#q Kv#i>U cOev#ni mgq
KŪv±#ii mvi#d#mi w`#K c^aevwnZ n#Z Pvq
,Aëvi#bwUs Kv#i>U Gi G cÖeYZv#K w<b B#d±
e#j|
eÿLÿt w<b G#d±i Kvi#b jvBb Zv#ii cÖ`'#"Q` K#g
hvq| d#j Aëvi#bwUs Kv#i>U cÖev#ni mgq KŪv±i
†iwR÷vÝ wKQzUv e,,w× cvq| Gi Kvib GKwU
wb#iU cwievwn AmsLÿ ÿz`^a ÿz`^a KYvi mgwó|
hLb Gai#bi cwievwn#Z Gwm mvcøvB cÖ#qvM
Kiv nq, ZLb cwievwni †K>`^a-'KYv,†jv evB#ii
mvi#dm A#cÿv AwaK msLÿK gÿM#bwUK d-†v<
Øviv cwi#ewóZ _v#K| ZvB D³ KYv,†jv#Z Avweó
†fv#ëR I wiqvK#UÝ Gi gvb ZzjbvgyjK †ewk nq |
GB Rb`†fZ#ii g#a`w`#q Kv#i>U bv wM#q mvi#dm
w`#q hvIqvi cÖevYZv †ekx †`Lv hvq|

W <b B#d± Wb#æœv~ Weiq, #jVI Dci Wb#t©I

K#it

1| cwievwn c`v_©t Gi ag© I ,Yv,#bi Dci |

2| Zv#ii eÿmt eÿm e,,w×i mv#_ mv#_ w<b

B#d± e,,w× cvq|

3| wd«Kz#qwÝt D"P wd«Kz#qwÝ#Z w<b

B#d± †ekx nh|

4| Zv#ii AvKvit mwjW KÛv±i A#cÿv

÷^av#ÛW Zv#ii w<b B#d± Kg| Zv#ii eÿm <

1cm Ges wd«Kz#qwÝ <50HZ n#j w<b B#d±

Kg nq|

1 | cÖw·wggwU B#d± Kv#K e#j?

DËit mgvšĭivj cwievnxØ#qi Kv#i>U hw` ci-úi
wecixZgyLx nq, Zvn#j Dfq Zv#ii
wbKUeZ©x As#k Kv#i>U †WbwmwU e,,w×
cvq| GKgyLx n#j `yieeZ©x As#k Kv#i>U
†WbwmwU e,,w× cvq, G ai#bi NUubv#K
cÖw·wggwU B#d± e#j|

cÖw·wggwU B#d#±i Kvi#b wK nq?

cÖw·wggwU B#d#±i Kvi#b cwievwni Kv#i>U
wefvRb cÖfvweZ nq Ges we#kl K#i

AvÛviMÖvDÛ Kve#ji †iwR÷vÝ e,,w× cvq|

THANK YOU